

# VP-Schaltung in SC-Technik

开关电源电路。之后讲解过原理，现在结合信号与系统中S变换和Z变换来研究  
S变换、 $G+j\omega$ 。并指出到目前为止变换不能满足的函数，例如指数函数。

Z变换。 $Z = e^{sT} \Leftrightarrow s = \frac{1}{T} \ln z$ ，Z变换得到的是取样信号。双边拉普拉斯变换

## 1. Allgemeine Grundlagen

主要用做采样和滤波

### 1.1. S变换基本性质

- 一时域定理： $\mathcal{L}[f^{(n)}(t)] = sF(s) - f(0-)$

- 积分定理： $\mathcal{L}[f(t)(t)] = \frac{1}{s} f'(0-) + \frac{1}{s^2} F(s)$

- 不变值定理： $f(0+) = \lim_{t \rightarrow 0^+} f(t) = \lim_{s \rightarrow \infty} sF(s)$ ,  $f'(0+) = \lim_{t \rightarrow 0^+} s[F(t) - f(0+)]$

- 终值定理： $f(t) \Leftrightarrow F(s)$ ,  $f(\infty) = \lim_{s \rightarrow 0} sF(s)$

常用ZS变换：

$$e^{at} \epsilon(t) \Leftrightarrow \begin{cases} \frac{1}{s-a}, \operatorname{Re}[s] > a \\ \text{无界, } a < a. \\ \text{不稳, } a = a. \end{cases} \quad e^{\beta t} \epsilon(-t) \Leftrightarrow \begin{cases} \text{无界, } \operatorname{Re}[s] = \beta > \beta \\ \text{不稳, } \beta = \beta \\ -\frac{1}{s-\beta}, \beta < \beta \end{cases}$$

$$g_2(t - \frac{T}{2}) \Leftrightarrow \frac{1 - e^{-sT}}{s}, \operatorname{Re}[s] > -\infty, \quad \delta(t) \Leftrightarrow 1, \quad \delta'(t) \Leftrightarrow s$$

$$\epsilon(t) \Leftrightarrow \frac{1}{s}, \operatorname{Re}[s] > 0, \quad e^{\beta t} \Leftrightarrow \frac{1}{s - j\beta}, \operatorname{Re}[s] > 0$$

其余性质见PDF → P238.

### 1.2. 电路网络在S域变换型，通过 $\sum I = 0$ , $\sum U = 0$ 及互易方程

$$(1) 电压  $\frac{1}{G} \quad U(s) = RI(s), \quad I(s) = GU(s)$$$

$$(2) 电感 L. \quad U = L \frac{di}{dt} \quad U(s) = sL I(s) - L i(0-), \quad I(s) = \frac{1}{sL} U(s) + \frac{i(0-)}{s}$$

$$(3) 容 C. \quad i = C \frac{du}{dt} \quad U(s) = \frac{1}{sC} \bar{U}(s) + \frac{U(0-)}{s} \quad I(s) = sC U(s) - C U(0-)$$

对于电感仅用串联等效或并联等效计算。

## 1.2. Z变换

常用Z变换

$$a^k \epsilon(k) \Leftrightarrow \begin{cases} \frac{z}{z-a}, |az^{-1}| < 1 \\ \text{不稳, } |a| = 1 \\ \text{无界, } |a| > 1. \end{cases} \quad b^k \epsilon(-k) \Leftrightarrow \begin{cases} \frac{-z}{z-b}, |z| < |b| \\ \text{不稳, } |b| = |b| \\ \text{无界, } |z| > |b|. \end{cases}$$

$$\epsilon(k) \Leftrightarrow \frac{z}{z-1}, |z| > 1. \quad \epsilon(-k-1) \Leftrightarrow \frac{-z}{z-1}, |z| < 1.$$

性质。PDF → P292.

- 双边变换  $f(k \pm m) \Leftrightarrow z^{\pm m} F(z)$

- 单边  $f(k-m) \Leftrightarrow z^{-m} F(z) + \sum_{k=0}^{m-1} f(k-m) z^{-k}$

- 双边积分  $k^n f(k) \Leftrightarrow [-z \frac{d}{dz}]^n F(z)$

- 双边积分  $\frac{f(k)}{k+m}, k+m > 0 \Leftrightarrow z^m \int_z^\infty \frac{F(\eta)}{\eta^{m+1}} d\eta$

- 不变值定理  $f(0) = \lim_{z \rightarrow \infty} F(z)$

$$f(m) = \lim_{z \rightarrow \infty} [F(z) - \sum_{k=0}^{m-1} f(k) z^{-k}]$$

$$f(\infty) = \lim_{z \rightarrow 1} \frac{z-1}{z-1} f(z)$$

1. 欧拉方法。1 近似解解方程(迭代, 较深)

2. 单边  $z = e^{sTs} \approx 1 + sTs \rightarrow sTs = z - 1$

3. 反复  $z^{-1} = e^{-sTs} = 1 - sTs \rightarrow sTs = 1 - z^{-1}$

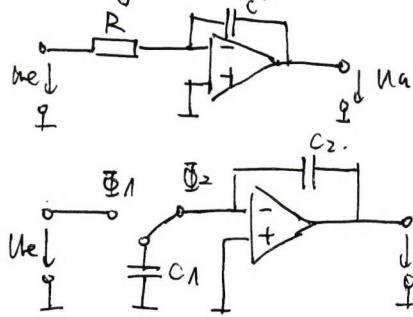
4. 双线性近似

$$sTs = \ln z = \frac{z-1}{z+1} \cdot 2,$$

$$z = e^{sTs} = \frac{e^{\frac{sTs}{2}}}{e^{-\frac{sTs}{2}}} = \frac{1 + \frac{sTs}{2}}{1 - \frac{sTs}{2}}$$

$$sTs = \frac{z-1}{z+1} \cdot 2$$

analog Integrator, 反馈接中性点向开环调查，接电容对积分器小信号无影响；



$$G(s) = \frac{U_a(s)}{U_{el}(s)} = \frac{-\frac{1}{sC_1} I(s)}{R I(s)} = -\frac{1}{s^2 C_1}, \text{ (这里求积分器)}$$

这里这个电路是一个理想的积分器，前级是保持3  
瞬态过程在采样时已经完成了。实际上时钟  
还有一个死区时间，所以m是可变的。

重1时， $C_1$ 充电。重2时， $C_1$ 上电压为0、电荷全部到 $C_2$ ，可以驱动电荷守恒计算。

allgemein

$$\sum_n C_n [U_{cn}(\bar{\theta}_1) - U_{sn}(\bar{\theta}_2)] = 0,$$

$$\text{(这里 } C_1 \cdot U_{c1}(\bar{\theta}_1) + C_2 U_{c2}(\bar{\theta}_1) = C_1 U_{c1}(\bar{\theta}_2) + C_2 U_{c2}(\bar{\theta}_2) \\ C_1 U_{el}(k-1) + C_2 U_{el}(k-1) = 0 - C_2 U_{el}(k))$$

采用双边Z变换。

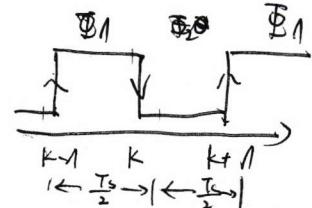
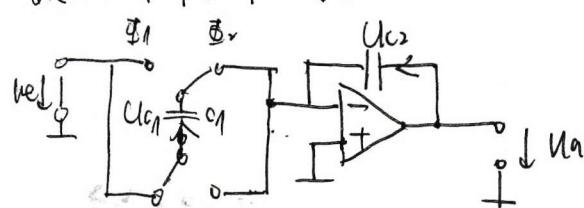
$$\Leftrightarrow C_1 \frac{1}{z} U_{el}(z) + C_2 \frac{1}{z} U_{el}(z) = -C_2 U_{el}(z) \Rightarrow U_{el}(z) = -\frac{C_1}{C_2} \cdot \frac{1}{z-1} U_{el}(z)$$

但是，电容必须做，时钟可调。缺点：时钟频率要高，信号有失真和衰减

## 9.2. SC-Integrator.

9.2.1. 改进方法。

9.2.2. 双线性近似



$$\text{列代数方程: } C_1 [-U_{el}(k-1) \rightarrow U_{el}(k)] + C_2 [U_{el}(k-1) - U_{el}(k)] = 0$$

$$\cancel{-C_1 U_{el}(z)} = C_1 U_{el}(z) \cancel{-C_1 U_{el}(z)}$$

$$-C_1 [\cancel{z^{-1} U_{el}(z)} + U_{el}(z)] + C_2 [z^{-1} U_{el}(z) - U_{el}(z)] = 0$$

$$U_{el}(z) C_2 (\frac{1}{z} - 1) = C_1 (\frac{1}{z} + 1) U_{el}(z) \Rightarrow \frac{U_{el}(z)}{U_{el}(z)} = -\frac{C_1}{C_2} \cdot \frac{z+1}{z-1}$$

$$\text{代入 } ST_s = 2 \frac{z-1}{z+1} \Rightarrow G(z) = -\frac{C_1}{C_2} \cdot \frac{2}{ST_s} = -\frac{1}{ST_s}, \text{ 其中 } z = \frac{C_1}{C_2} \cdot \frac{T_s}{2}$$

## 9.3. SC-Biquard-Filter.

= PLL电路、滤波系统的基本模型：

$$G(z) = -\frac{k_0 + k_1 z + k_2 z^2}{w_0 p^2 + \frac{w_0}{Q} z + z^2}, \quad G(z_0) = -\frac{a_0 + a_1 z_0 + a_2 z_0^2}{1 + \frac{z_0}{Q} + z_0^2} = \frac{U_a(z_0)}{U_e(z_0)}, \quad z_0 = \frac{s}{w_0}$$

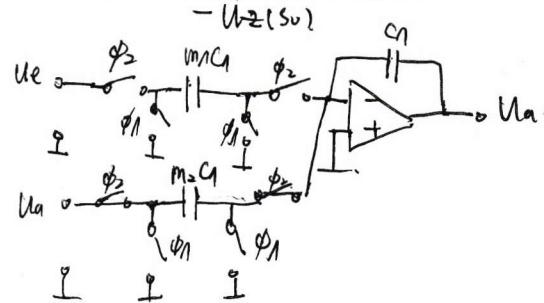
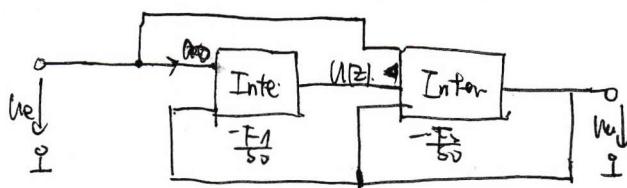
通过极点来判定滤波器的类型。 $a_1 = 0, a_2 = 0$ ，则为低通。

双阶滤波器，对于不同的Q值有不同的阶跃滤波器表二成

$$\underline{U_a(z_0)} \left[ 1 + \frac{z_0}{Q} + z_0^2 \right] = -[a_0 + a_1 z_0 + a_2 z_0^2] \underline{U_e(z_0)}$$

$$\begin{aligned} \underline{U_a(z_0)} &= - \left[ \underline{U_e(z_0)} \cdot \frac{z_0}{Q} + \underline{U_e(z_0)} \cdot \frac{z_0^2}{Q^2} + a_0 \underline{U_e(z_0)} + a_1 z_0 \underline{U_e(z_0)} + a_2 z_0^2 \underline{U_e(z_0)} \right], \quad \text{除 } z_0^2, \text{ 得 } \underline{U_a(z_0)} \text{ 和 } z_0^2 \underline{U_e(z_0)} \text{ 互换} \\ &= -\frac{1}{z_0} \left[ \frac{\underline{U_a(z_0)}}{Q} + (a_0 + a_2 z_0) \underline{U_e(z_0)} + \frac{1}{z_0} (a_0 \underline{U_e(z_0)} + \underline{U_a(z_0)}) \right]. \end{aligned}$$

$-\frac{1}{z_0}$  代表一个积分器



SC-01.

假设用  $U_{e1}$  和  $U_{e2}$  认为不变。  
由于  $\phi_1$  变化为单向脉冲，所以方程成立。

III.  $\phi_1$ : 只有  $C_3, C_2, \text{并联}$ ,  $\phi_2$ : ~~只由  $C_2$~~  加入  $C_1$ .

$$\Rightarrow C_3 U_{e2}(\phi_1) + C_2 U_{e1}(\phi_1) = C_3 U_{e3}(\phi_2) + C_2 U_{e2}(\phi_2) + C_1 U_{e1}(\phi_2)$$

$$\Rightarrow -C_3 U_{e2}(\phi_1) - C_2 U_{e1}(\phi_1) = -C_3 U_{e3}(\phi_2) - C_2 U_{e1}(\phi_2) - C_1 U_{e1}(\phi_2)$$

$$\phi_1 \rightarrow k-1 \quad \phi_2 \rightarrow k.$$

$$\Rightarrow -\frac{1}{2} C_3 U_{e2}(z) + \frac{1}{2} C_2 U_{e1}(z) = C_3 U_{e3}(z) + C_2 U_{e2}(z) + C_1 U_{e1}(z)$$

$$-\left(1 - \frac{1}{2}\right) C_2 U_{e1}(z) = \left(1 - \frac{1}{2}\right) C_3 U_{e2}(z) + C_1 U_{e1}(z)$$

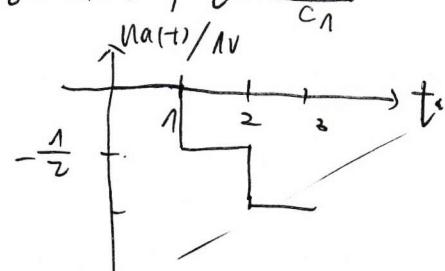
$$\underline{U}_{e1}(z) = -\frac{C_3}{C_2} \underline{U}_{e2}(z) + \frac{C_1}{C_2} \frac{1/z - 1}{z-1} \underline{U}_{e1}(z), \text{ 可以直接写结果。}$$

$$\text{从 Nernst ETTLER Rückwärts } STs = 1 - z^{-1} = \frac{z-1}{z}$$

$$\underline{U}_{e1}(s) = -\frac{C_3}{C_2} \underline{U}_{e2}(s) - \frac{C_1}{C_2} \frac{1}{STs} \underline{U}_{e1}(s)$$

$$(2) \text{ 假设 } \underline{U}_{e1}(s) = -\frac{C_1}{C_2} \cdot \frac{1}{STs} \underline{U}_{e1}(s) = -\frac{1}{8T} \underline{U}_{e1}(s), T = \frac{C_2 \cdot Ts}{C_1}$$

$$\Rightarrow \text{mit } 2 = Ts \frac{C_2}{C_1} = 100 \mu s \quad \underline{U}_{e1}(t) = -\frac{t}{T} \underline{U}_{e1}(0)$$

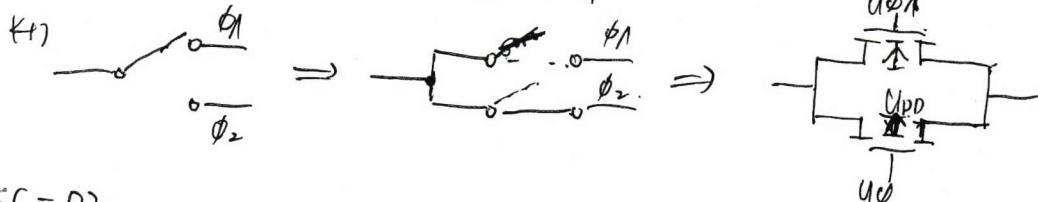


(3) 先求  $\underline{U}_{e2}(z)$  和  $\underline{U}_{e1}(z)$ .

$$C_2 \underline{U}_{e1}(z) = C_2 \cdot \frac{1}{z} \cdot \underline{U}_{e1}(z) + C_1 \cdot \frac{1}{z} \underline{U}_{e1}(z)$$

$$\Rightarrow \underline{U}_{e2}(z) = \frac{1}{z-1} \cdot \frac{C_1}{C_2} \cdot \underline{U}_{e1}(z) = \underline{U}_{e1}(z)$$

$$\Rightarrow \underline{U}_{e1}(z) = -\frac{C_3}{C_2} \underline{U}_{e2}(z) + \frac{C_1}{C_2} \frac{1}{z-1} \underline{U}_{e1}(z), \text{ mit Vorhätts. } STs = z-1.$$



SC-02

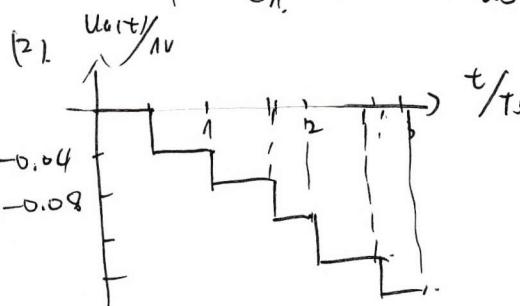
$$\text{III. } C_1 U_{e1}(\phi_1) + C_2 U_{e2}(\phi_1) = C_1 U_{e1}(\phi_2) + C_2 U_{e2}(\phi_2)$$

$$-C_1 U_{e1}(k-1) + C_2 U_{e2}(k-1) = C_1 U_{e1}(k) + C_2 U_{e2}(k)$$

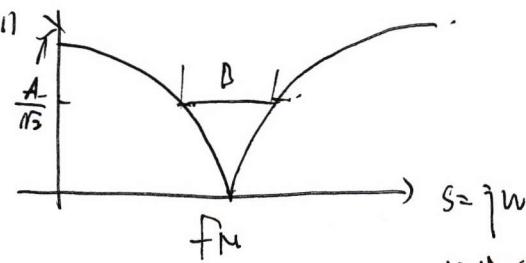
$$C_1 U_{e1}(k-1) - C_2(1 - \frac{1}{z}) = C_1(1 + \frac{1}{z}) U_{e2}(z)$$

$$\frac{U_{e1}(z)}{U_{e2}(z)} - \frac{C_1(z+1)}{C_2(z-1)} = -\frac{C_1}{C_2} \cdot \frac{z+1}{z-1} = -\frac{C_1}{C_2} \cdot \frac{4}{3}, \frac{STs}{z} = \frac{z-1}{2T}, T_s = \frac{T_0}{2}$$

$$\Rightarrow 2 = \frac{T_0}{4} \cdot \frac{C_2}{C_1}, \frac{1}{2} = 0.04 \frac{1}{\mu s}$$



SC-03.



$$s_0 = \frac{j}{\omega_p}, \text{ f\"ur } s = s_N: s_0 = j(\omega_N / \omega_p) / j(\omega_p)$$

$$\Rightarrow s_0 = j, ; G(s_0) = 0.$$

$$\Rightarrow G(s_0 = j) = \frac{a_0 + a_1 j + a_2 j^2}{1 + \frac{j}{Q} + j^2} = 0 \Rightarrow jQ(a_0 - a_2 + j a_1)$$

$$\Rightarrow a_1 = 0, a_0 = a_2.$$

赵中行  $G(j) = -1, a_0 = a_2 = 1, a_1 = 0.$

$$f_{s_0} = \frac{f_N \cdot \omega_0}{\omega_p}, T_{s_0} = \frac{\omega_0 \omega_p}{\omega_p \cdot f_s} = \frac{f_N \cdot 2\pi}{f_s} = 0.1 + j1$$

$$(2) \underline{U_a}(s_0) = \frac{1}{s_0} [s_0 \underline{U_e}(s_0) + \frac{1}{s_0} [\underline{U_e}(s_0) + (1 + \frac{s_0}{Q}) \underline{U_a}(s_0)]]$$

$$\underline{U}_Z = 0 - \frac{1}{s_0} [\underline{U_e}(s_0) + (1 + \frac{s_0}{Q}) \underline{U_a}(s_0)], \text{ 用 SC-01. (1)}$$

$$\underline{U_a}(s_0) = -\frac{1}{s_0} [s_0 \underline{U_e}(s_0) - \underline{U}_Z(s_0)]. \text{ 用 SC-01. (2)}$$

$$s_0 = 8\pi \rightarrow \frac{1}{s_0} = \frac{1}{8\pi} \cdot \frac{1}{2} = \frac{1}{16\pi} \text{ rad/s}$$

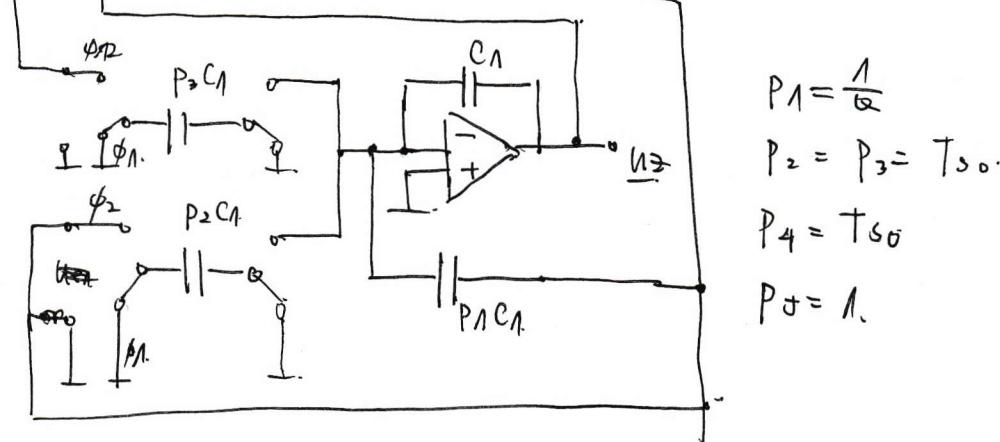
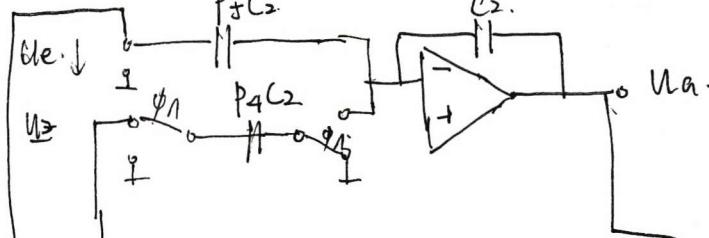
$$1.(1) \underline{U_a}(s) = -\frac{C_3}{C_2} \underline{U_{e2}}(s) - \frac{C_1}{C_2} \frac{1}{sT_s} \underline{U_{e1}}(s)$$

$$1.(2) \underline{U_a}(s) = -\frac{C_3}{C_2} \underline{U_{e2}}(s) + \frac{C_1}{C_2} \frac{1}{sT_s} \underline{U_{e1}}(s)$$

$$\left. \begin{aligned} & \frac{C_1}{C_2} = 1 + \frac{s_0}{Q} \\ & \frac{C_3}{C_2} = 1, \underline{U_{e2}} = \underline{U_e}, \underline{U_{e1}} = \underline{U_a} \\ & P_1 C_1 = P_2 C_1 \\ & P_3 C_1 \rightarrow P_2 = P_3 \\ & P_4 C_2 \\ & P_5 C_2 \end{aligned} \right\}$$

$$-\frac{1}{s_0} [\underline{U_e}(s_0) + \underline{U_a}(s_0)] - \frac{1}{Q} \underline{U_a}(s_0) = -\frac{C_3}{C_2} \underline{U_{e2}}(s) - \frac{C_1}{C_2} \cdot \frac{1}{sT_s} \underline{U_{e1}}(s),$$

$$-\underline{U_e}(s_0) + \frac{1}{s_0} \underline{U}_Z(s_0) = -\frac{C_3}{C_2} (\underline{U_{e2}}(s)) + \frac{C_1}{C_2} \frac{1}{sT_s} (\underline{U_{e1}}(s)).$$



$$P_1 = \frac{1}{Q}$$

$$P_2 = P_3 = T_{s_0}$$

$$P_4 = T_{s_0}$$

$$P_5 = 1.$$