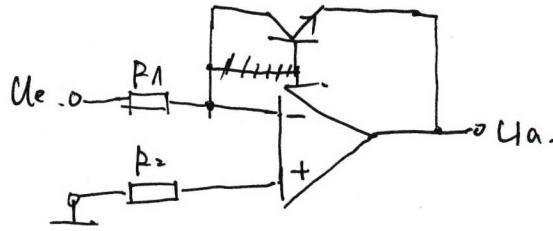


Logarithmierungsschaltung



$U_{DC} \neq 0$. 沒有截止效應，即 T 不管工作在何處。

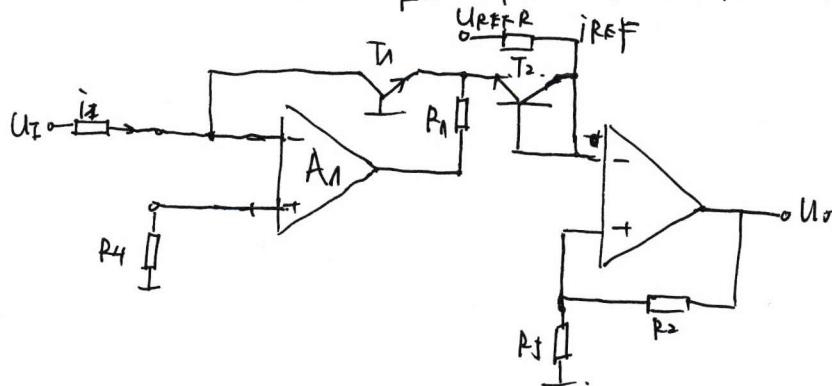
$$\frac{U_E}{R_1} = i_C \rightarrow i_E = i_C = I_S \exp\left(\frac{U_{BE}}{kT}\right), \text{ 且 } U_{BE} = -U_A.$$

$$U_{BE} = -U_A = U_T \ln \frac{I_E}{I_S}$$

中性點決定 I_S , U_T , 及溫度影響

I_S 可以由 $\ln \frac{I_E}{I_S}$ 做差，即去 T_{PM} 需要一個溫度 P_0 ，

$$U_0 = \frac{R_1}{R_2} \cdot U_T \ln \frac{I_E}{I_{E0}} - (T + \text{校正項}) \cdot \text{用熱敏電阻補償 } U_T.$$



$$\cdot T_1, U_{BE1} = 0 \quad T_2, U_{BE2} = 0.$$

$$\cdot U_0 = k \cdot (U_{BE2} - U_{BE1})$$

$$\frac{U_0}{R_1 + R_2} \cdot R_2 = U_{BE2} - U_{BE1} \Rightarrow U_0 \approx \left(1 + \frac{R_2}{R_1}\right) U_T \ln \frac{I_E}{I_{E1} \cdot I_{E2}}$$

又 η 為常數。

$$U_x = \frac{R_2}{R_1 + R_2} U_0 = U_{BE1} - U_{BE2} = U_T \ln \frac{I_{E1}}{I_S} - \ln \frac{I_{E2}}{I_S}$$

$$U_0 = 23 \left(1 + \frac{R_2}{R_1}\right) U_T \ln \frac{I_{E1}}{I_{E2}} \leftarrow \begin{cases} k \ln x = \ln x \\ \ln x = \frac{k}{23} \end{cases} \xrightarrow{\text{換底公式}} \begin{cases} \frac{\eta}{23} = \frac{k}{T_0} \\ \ln x = \eta \end{cases} \Rightarrow x = e^{\eta} = e^{\frac{\eta}{23}} = e^{\frac{k}{T_0}} = e^{\frac{k}{T_0} \cdot 10} = e^{10 \cdot \frac{k}{T_0}}$$

用 R_2 來控制 U_T 。

$$R_2(T) = R_{20} [1 + T_C(T - T_0)] \quad U_T = \frac{kT}{Q} = U_{T0} \cdot \frac{T}{T_0}$$

$$T_C = \frac{d}{dT} \left(1 + \frac{R_1}{R_2}\right) \cdot U_T = 0 \Rightarrow \frac{U_{T0}}{T_0} + R_1 \cdot \frac{U_{T0}}{R_{20}} \cdot \left[\frac{T}{1 + T_C(T_0 - T_0) \cdot T_0} \right]$$

$$\Rightarrow U_T' + R_1 \cdot \frac{U_{T0} \cdot R_2 - R_2 \cdot U_T}{[R_2]^2} = \left(1 + \frac{R_1}{R_2}\right) U_T' - \frac{R_1}{R_2} \cdot U_T \cdot R_2 \cdot T_C = 0$$

$$\left(1 + \frac{R_1}{R_2}\right) \frac{U_{T0}}{T_0} - \left(\frac{R_1}{R_2}\right)^2 \frac{U_{T0}}{T_0} \cdot T \cdot R_2 \cdot T_C = 0 \Rightarrow T_C =$$

$$1 + \frac{R_1}{R_2} - \frac{R_1}{R_2} \cdot \frac{T_C \cdot T_0}{1 + T_C(T - T_0)} \Rightarrow \frac{R_1}{R_2} \cdot \frac{1 + T_C(T - T_0)}{1 + T_C(T - T_0) + 1} = 0$$

$$1 - T_C \cdot T_0 = -\frac{R_1}{R_2} - \frac{R_2}{R_1} T_C \cdot (T - T_0) \quad |_{T=T_0} = \left(1 + \frac{R_2}{R_1}\right) / T_0 = T_C \times \text{用來改變 } R_2$$

Verstärker mit Dioden in der Gegenkopplung. A-种对数放大器.

$$i_D = I_S \exp \frac{U_T}{U_T} \Rightarrow U_D = U_T \ln \frac{I_D}{I_S}$$

$$U_{A1} = -(U_{D1} + U_{D2}) = -2 U_T \ln \frac{I_D}{I_{ref}}$$

$$U_{A2} = U_{D3} + U_{D4} = 2 U_T \ln \frac{I_D}{I_{ref}}$$

$$U_A = -\frac{R_2}{R_1} (U_{A1} + U_{A2}) = -\frac{R_2}{R_1} \left[-2 U_T \left(\ln \frac{I_D}{I_{ref}} \cdot \frac{I_F}{I_{ref}} \right) \right]$$

$$= \frac{R_2}{R_1} \cdot 2 U_T \ln \frac{I_D}{I_{ref}} = 4.6 \frac{R_2}{R_1} U_T \ln \frac{I_D}{I_{ref}}$$

Temperaturabhängigkeit:

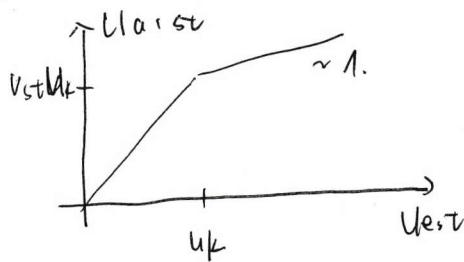
$$\delta U_A = \frac{d U_A}{dT} \delta T = 4.6 \frac{R_2}{R_1} \ln \left(\frac{I_D}{I_{ref}} \right) \cdot \frac{U_{TO}}{T_0} \delta T$$

R_1 与 T 成反比， R_2 与 T 成正比。

$$d \frac{U_T}{R_1} \Big|_{T=T_0} = 0 \Rightarrow$$

$$\frac{U_{TO} \cdot R_1 - U_T \cdot R_{10} \cdot T_C}{(R_1)^2} \Big|_{T=T_0} = \frac{T_C - \frac{1}{T_0} U_{TO}}{\frac{1}{R_{10}} U_{TO}} = 0 \quad T_C = \frac{1}{T_0} = 3.33 \times 10^{-3} K^{-1} \quad \text{形成负反馈。}$$

"A/I - Verstärker"



$$U_{A2} = \begin{cases} V_{st-West} & 0 \leq U_{st} \leq U_K \\ (V_{st-A}/U_K + U_{est}) U_K < U_{st} \end{cases}$$

$L_0 = 0.1$

$$1.5 \times 10^3 \rightarrow 1.5 \times 10^{-4}$$

$$(1) U_{BA} = \frac{R_4}{R_3 + R_4}, U_{A1} = U_{BE1} - U_{BE2} = U_T \ln \frac{I_F}{I_{ref}}$$

$$\Rightarrow U_{A1} = \left(1 + \frac{R_3}{R_4} \right) U_T \ln \frac{I_F}{I_{ref}}$$

$$(2) \frac{\partial U_{A1}}{\partial T} \Big|_{T=T_0} = 0 \Rightarrow \ln \frac{I_F}{I_{ref}} \left[\frac{U_{TO}}{T_0} + R_3 \cdot \frac{\frac{U_{TO} \cdot R_4 - R_4' U_T}{(R_4)'}}{(R_4)'^2} \right] \Rightarrow \ln \frac{I_F}{I_{ref}} \left[\frac{U_{TO}}{T_0} + \frac{R_3}{R_{40}} \left(\frac{U_{TO}}{T_0} \frac{R_4 - R_4' U_T}{(R_4)'^2} \right) \right]$$

$$\Rightarrow \frac{\partial U_{A1}}{\partial T} \Big|_{T=T_0} = \ln \frac{I_F}{I_{ref}} U_{TO} \left(\frac{1}{T_0} + m \frac{1}{T_0} - m T_{C4} \right), \quad m = \frac{R_3}{R_4}$$

$$\Rightarrow \frac{m+1}{T_0} = m T_{C4} \Rightarrow m = \frac{1}{T_{C4} - T_0 - 1} = \frac{1}{10.5 - 1} \neq \frac{1}{1.05 - 1} = 2.6$$

$$(3), P_L = 1 \times 10^{-3} W = 1 mW \quad 0 dBm \quad P_H = 10 mW \triangleq 10 dBm$$

$$P_R = P_S - d.S [dBm] \quad P_{R,mW} = 1 mW \cdot \frac{P_S - d.S}{10^{10}} \Rightarrow$$

$$S = 10 km, \quad P_{PL} = -10 dBm = 0.1 mW \Rightarrow I_{FL} = 1 \times 10^{-4} \times 0.1 = 10^{-5} A = 10 \mu A$$

$$P_{PH} = 0 dBm - 1 mW \Rightarrow I_{FH} = 10 \mu A$$

$$S = 70 \text{ km} \quad P_{p2} = 0 - 70 \text{ dB} = -70 \text{ dBm} = 1 \times 10^{-3} \times 10^{-7} = 10^{-10} \text{ W} \quad I_{F-L} = 50 \text{ pA} \\ \Rightarrow I_{F-H} = 50 \text{ pA}$$

4) $\boxed{P_H = 10 \text{ mW} = 10 \text{ dBm} \Rightarrow I_{F-max} = 5 \times 10^{-4} \text{ A}}$

$$U_{a1} = (1+m)U_T \ln \frac{I_{Fmax}}{I_{REF}} \Rightarrow \frac{I_{Fmax}}{I_{REF}} = e^{\frac{U_{a1}}{(1+m)U_T}}$$

$$I_{REF} = \frac{I_{Fmax}}{e^{\frac{U_{a1}}{(1+m)U_T}}} = \frac{5 \times 10^{-4}}{e^{51-26 \times 10^{-3}}} = 80.1 \text{ nA}$$

5).

$$\Delta U_{a2} = \Delta U_{a1} - \left(\frac{R_1 + R_2}{R_1} \right) = \Delta U_{a1} + 1 + \frac{R_2}{R_1}$$

$$\Delta U_{a1} = (1+m)U_T \left[\ln \frac{I_{Fmax}}{I_{REF}} - \ln \frac{I_{Fmin}}{I_{REF}} \right] = (1+m)U_T \ln 10 = 2.3(1+m)U_T = 1.278$$

$$\frac{R_2}{R_1} = \frac{\Delta U_{a2}}{\Delta U_{a1}} - 1 = 6.99 \approx 1.$$

L0-02.

$$1) U_{a1} = -(U_{D1} + U_{D2}) = -2U_T \ln \frac{I_e}{I_{D0}} \quad U_{a2} = 2U_T \ln \frac{I_{REF}}{I_{D0}}$$

~~$$U_{a1} = \frac{R_2}{R_1} \cdot (U_{a1} + U_{a2}) = \frac{R_2}{R_1} (2U_T \ln \frac{I_{REF}}{I_e}) \Rightarrow \frac{R_2}{R_1} = 2U_T \ln \frac{I_e}{I_{REF}}$$~~

$$2) I_{D1} = I_{D2} \Rightarrow U_a = 2 \cdot 6 \frac{R_2}{R_1} U_T \ln \frac{I_e}{I_{REF}}$$

~~$$3) U_{a1} = U_{a1} |_{10T_e} - U_{a1} |_{T_e} = 4.6 \frac{R_2}{R_1} U_T \ln \frac{10I_e}{I_e} = 4.6 \frac{R_2}{R_1} U_T$$~~

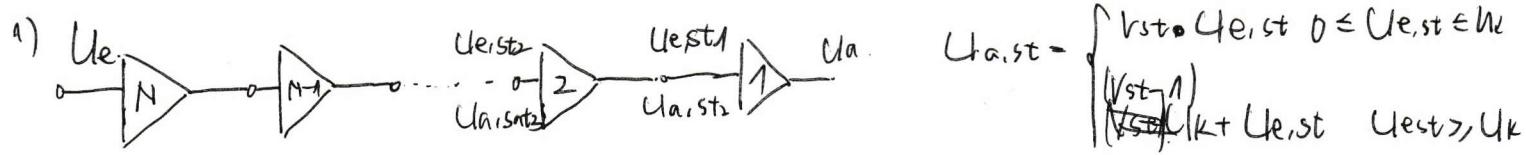
~~$$3) I_{e,max} = I_{e,min} \cdot 10^3 \quad 1V = \frac{R_2}{R_1} \cdot U_T \cdot 4.6 \ln \frac{10^{-4}}{I_{REF}} \Rightarrow 1 \times 10^{-4} \cdot 1 \times 10^{-7} = I_{REF}^2 \\ \Rightarrow I_{REF} = 3.16 \text{ nA}$$~~

4). Ans Vortlesung - Skript:

$$\text{Werm. } T_c = \frac{1}{T_0} \quad \frac{\partial I_a}{\partial T} \Big|_{T=T_0} = 0 \\ = 0.0033 \text{ } \text{A/K}$$

Ans die Gleichung, die Temperatur ist abhängig von U_T . und I_s von $\ln \frac{I_{D1}}{I_s} - \ln \frac{I_{D2}}{I_s}$ kam die Anpassung von I_s kompensiert. mit I_s nicht zu tun. für $U_T \approx T$. muss von einer Temperaturabhängige Widerstände kompensiert werden. ($1 + \frac{M}{P_2} U_T$ oder $\frac{P_1}{P_2} U_T$. [P_2 ist abhängig von Temp].)

L0 - 03.



2) $U_{e,st_1} = U_{a,st_2} = U_k$. $Vst = 4 > 1$. Alle $U_e \leq U_k$

$$\Rightarrow U_{e,1} = U_{a,st_1} = \frac{U_k}{Vst^{N-1}} = 97.7 \text{ mV}$$

$$U_a = V \cdot U_k = 400 \text{ mV}$$

3). $U_{e,2} = \frac{U_k}{Vst^{N-2}} = 390.6 \text{ mV}$

$$U_a = U_k \cdot Vst + (Vst-1) U_k = 2(Vst-1) U_k = U_k \cdot 700 \text{ mV}$$

4) $U_{e,3} = \frac{U_k}{Vst^{N-3}} = 1.16 \text{ mV}$ $U_{a,3} = 1 \text{ V}$

5) $U_{e,i} = \frac{U_k}{Vst^{N-i}}$ $U_{a,i} = [4 + 2(i-1)] U_k$
 $= [(Vst-1)i + 1] U_k$.

6) $\frac{U_{e,i}}{U_{e,i-1}} = \frac{Vst^{N-(i-1)}}{Vst^{N-i}} = Vst$ $\Delta U_a = (Vst-1) U_k = 300 \text{ mV}$

$$U_e = \lg Vst = 0.6$$
 $U_a \cdot \lg = \frac{(Vst-1) U_k}{0.6} = 500 \text{ mV}$

7) $U_a = \frac{\Delta U_a}{\Delta U_e} \lg \frac{U_e}{U_{ref}} = \alpha U \cdot \lg \frac{U_e}{U_{ref}} + U_{a,i-1}$

i = 1

$$Vst \cdot U_k = (Vst-1) U_k \cdot \lg \left[\frac{U_e}{U_{ref}} \cdot \frac{Vst^{N-1}}{Vst} + Vsr \right]$$

$$Vst \cdot U_k = (Vst-1) U_k \cdot \lg \left[\frac{U_k Vst^{N-2}}{U_{ref} Vst^{N-1}} + \frac{U_k / U_{ref}}{Vst-1} \right]$$

$$Vst \cdot U_k \cdot \lg Vst = (Vst-1) U_k \cdot \lg \frac{U_k}{Vst-1}$$

$$U_{ref} = \frac{U_k}{Vst} \cdot 10 - \frac{Vst \cdot U_k}{Vst-1} \cdot \frac{Vst-1}{Vst}$$

$$U_{ref} \cdot 10 = \frac{Vst \cdot \lg Vsr}{Vst-1} = \frac{U_k}{Vst}$$

$$\Rightarrow 1.137 \times 10^{-3} \text{ V}$$

$$1.137 \text{ mV}$$